

In the Name of God



DYNAMICS

[Course No. 8102128]

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بناام خدا



دینامیک (نیمسال ۲-۹۷-۹۶)

شماره درس ۸۱۰۲۱۲۸



دکتر مهدی قاسمیه
دانشکده مهندسی عمران

فصل نہم :

Mechanical Vibration

ارتعاشات مکانیکی

Free vibration ارتعاش آزاد ذره یا نقطه مادی (بدون نیروی خارجی)

ارتعاش آزاد نامیرا

ارتعاش آزاد آونگ ساده

ارتعاش آزاد جسم صلب

Conservation of energy اصل حفظ انرژی مکانیکی

Forced vibration ارتعاش زوری (با نیروی خارجی)

Damped free vibration ارتعاش آزاد با میرائی

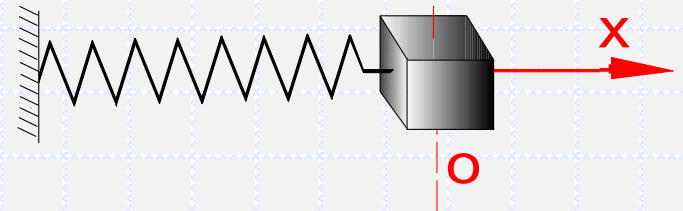
Damped forced vibration ارتعاش زوری با میرائی

Free Vibrations of Particles (Simple Harmonic Motion)

ارتعاش آزاد ذره یا نقطه مادی (بدون نیروی خارجی)

$$f = -kx$$

Mass on a Horizontal spring



$$m \ddot{x} = -kx$$

$$\ddot{x} + \frac{k}{m} x = 0$$

Differential Equation

$$\ddot{x} + \omega_n^2 x = 0 \quad \omega_n \text{ is the natural circular frequency}$$

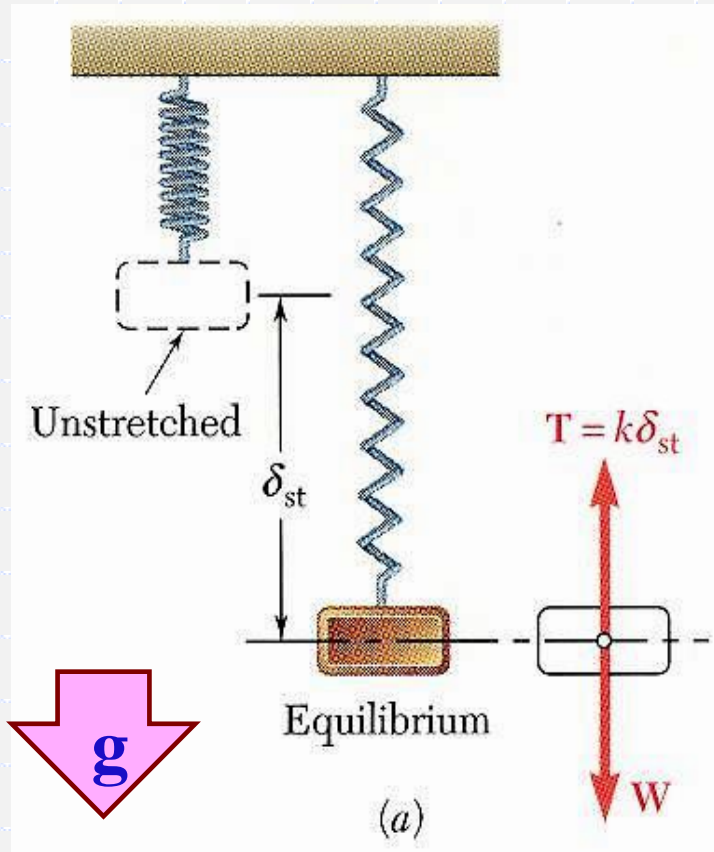
$$x = A \sin \left(\sqrt{\frac{k}{m}} t \right) + B \cos \left(\sqrt{\frac{k}{m}} t \right)$$

$$\omega_n = \sqrt{\frac{k}{m}}$$

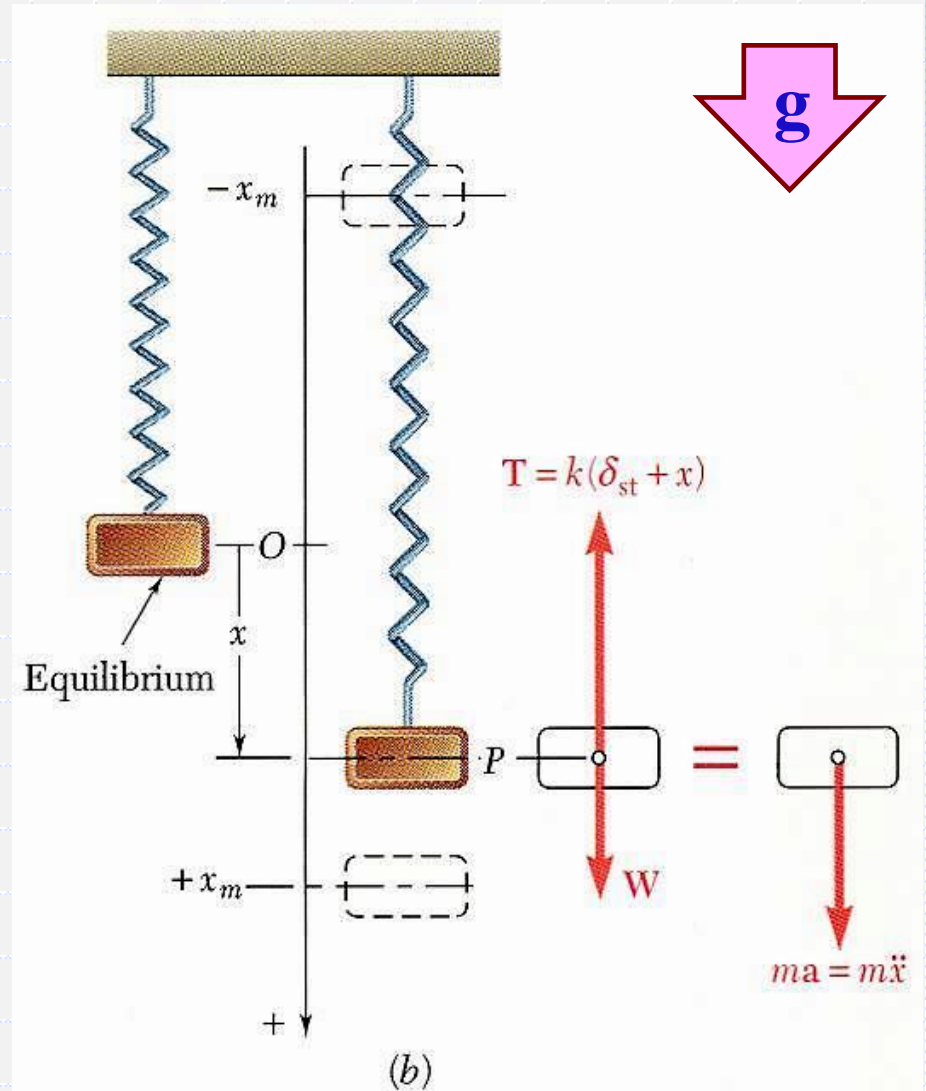
$$A = v_0 / \omega_n$$

$$B = x_0$$

Mass on a Vertical spring



$$W = T = k\delta_{st}$$



- If a particle is displaced through a distance x_m from its equilibrium position and released with no velocity, the particle will undergo *simple harmonic motion*,

$$ma = F = W - k(\delta_{st} + x) = -kx$$

$$m\ddot{x} + kx = 0$$

- General solution is

$$x = A \sin\left(\sqrt{\frac{k}{m}} t\right) + B \cos\left(\sqrt{\frac{k}{m}} t\right)$$

$$= A \sin(\omega_n t) + B \cos(\omega_n t)$$

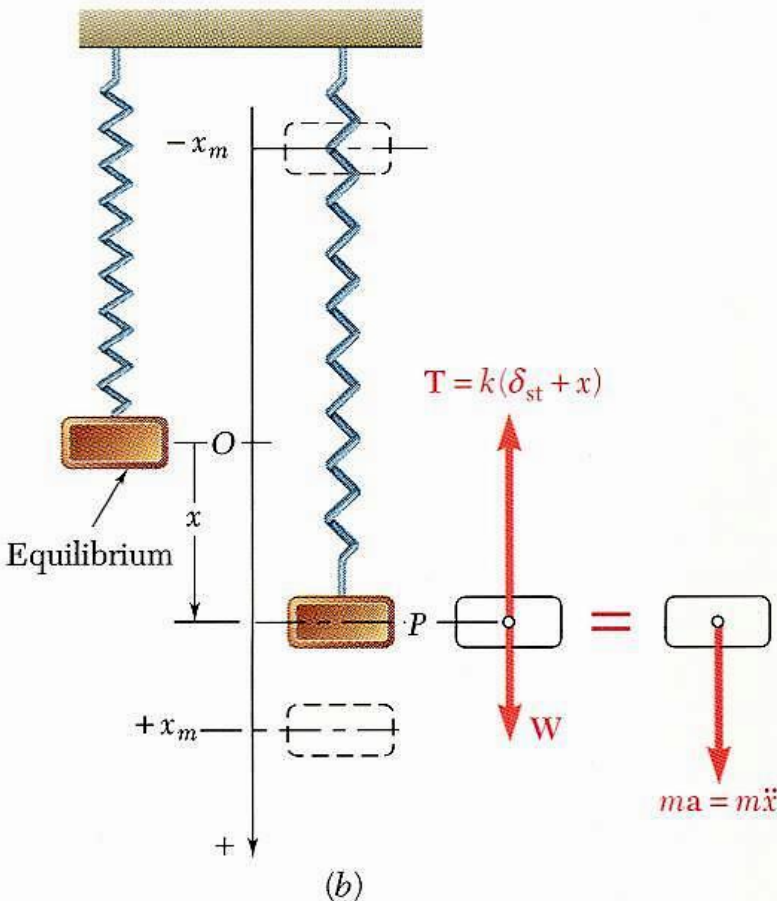
- x is a *periodic function* and ω_n is the *natural circular frequency* of the motion.

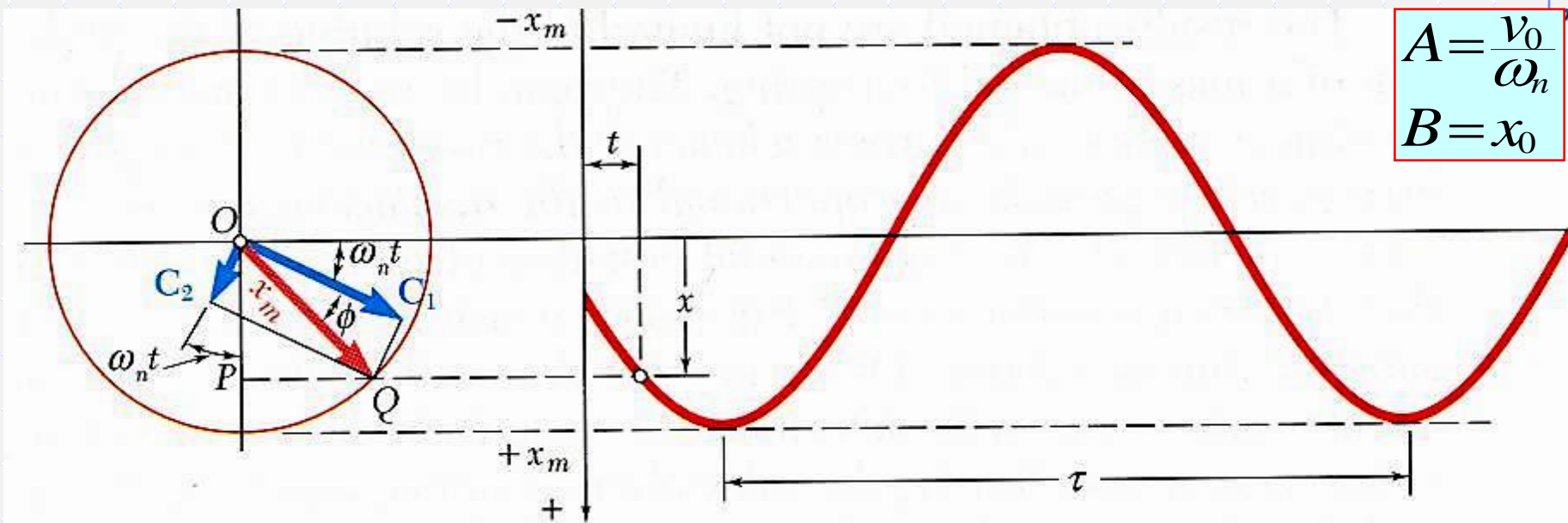
$$\omega_n = \sqrt{\frac{k}{m}}$$

- A and B are determined by the initial conditions:

$$x = A \sin(\omega_n t) + B \cos(\omega_n t) \quad B = x_0$$

$$v = \dot{x} = A\omega_n \cos(\omega_n t) - B\omega_n \sin(\omega_n t) \quad A = v_0/\omega_n$$





$$A = \frac{v_0}{\omega_n}$$

$$B = x_0$$

- Displacement is equivalent to the x component of the sum of two vectors $\vec{C}_1 + \vec{C}_2 = \vec{A} + \vec{B}$ which rotate with constant angular velocity ω_n .

$$x = x_m \sin(\omega_n t + \phi)$$

$$x_m = \sqrt{(v_0/\omega_n)^2 + x_0^2} = \text{amplitude}$$

$$\phi = \tan^{-1}(v_0/x_0\omega_n) = \text{phase angle}$$

$$\tau_n = \frac{2\pi}{\omega_n} = \text{period}$$

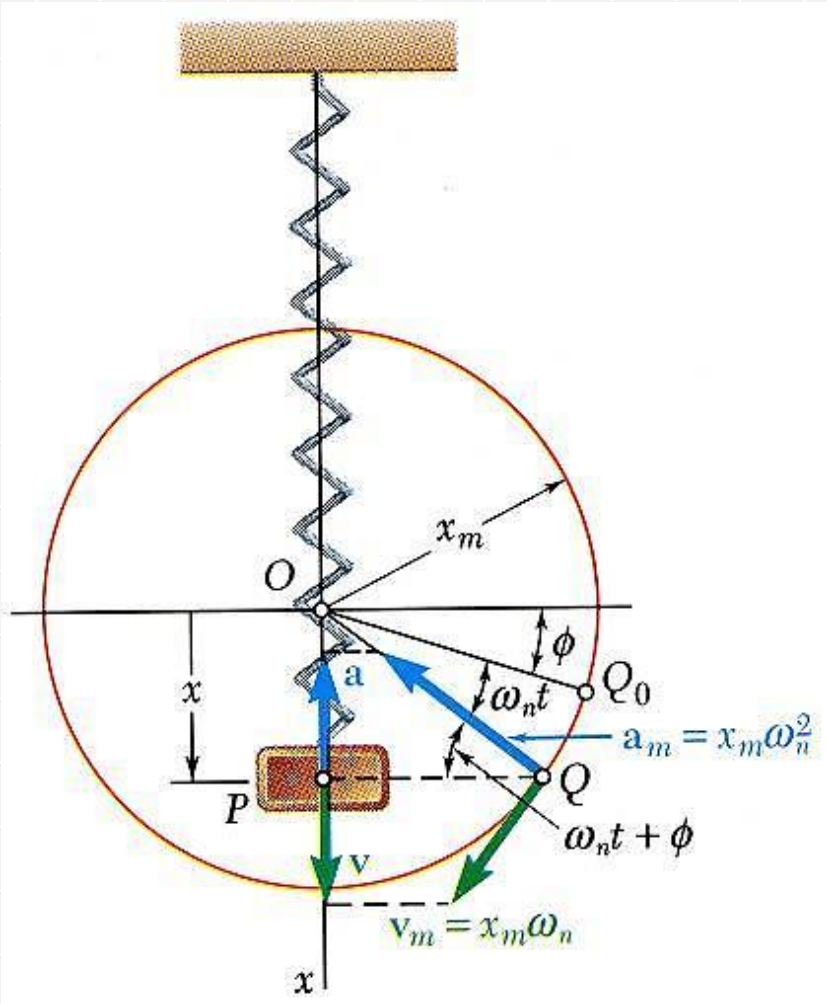
$$f_n = \frac{1}{\tau_n} = \frac{\omega_n}{2\pi} = \text{natural frequency}$$

- Velocity-time and acceleration-time curves can be represented by sine curves of the same period as the displacement-time curve but different phase angles.

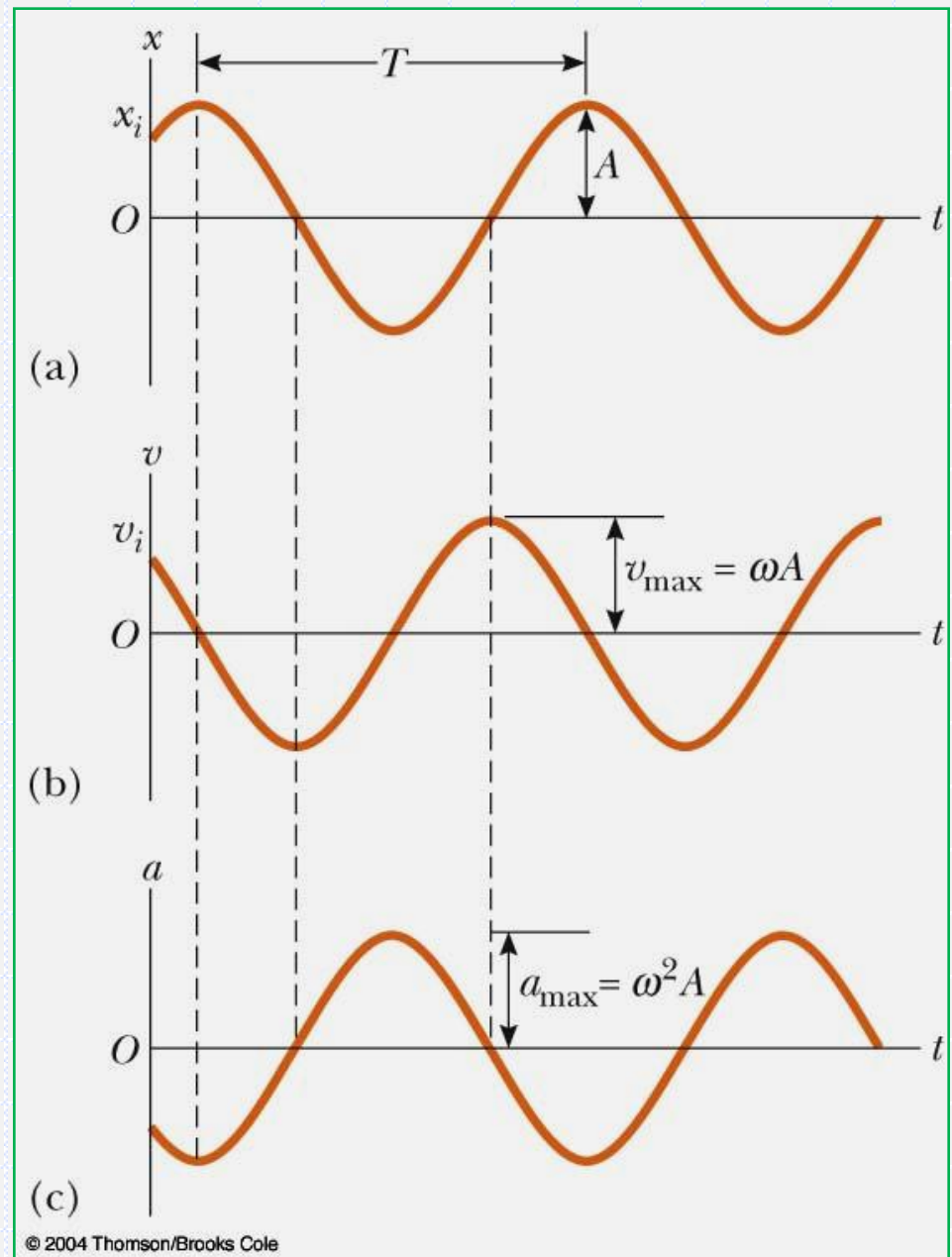
$$x = x_m \sin(\omega_n t + \phi)$$

$$\begin{aligned} v &= \dot{x} \\ &= x_m \omega_n \cos(\omega_n t + \phi) \\ &= x_m \omega_n \sin(\omega_n t + \phi + \pi/2) \end{aligned}$$

$$\begin{aligned} a &= \ddot{x} \\ &= -x_m \omega_n^2 \sin(\omega_n t + \phi) \\ &= x_m \omega_n^2 \sin(\omega_n t + \phi + \pi) \end{aligned}$$

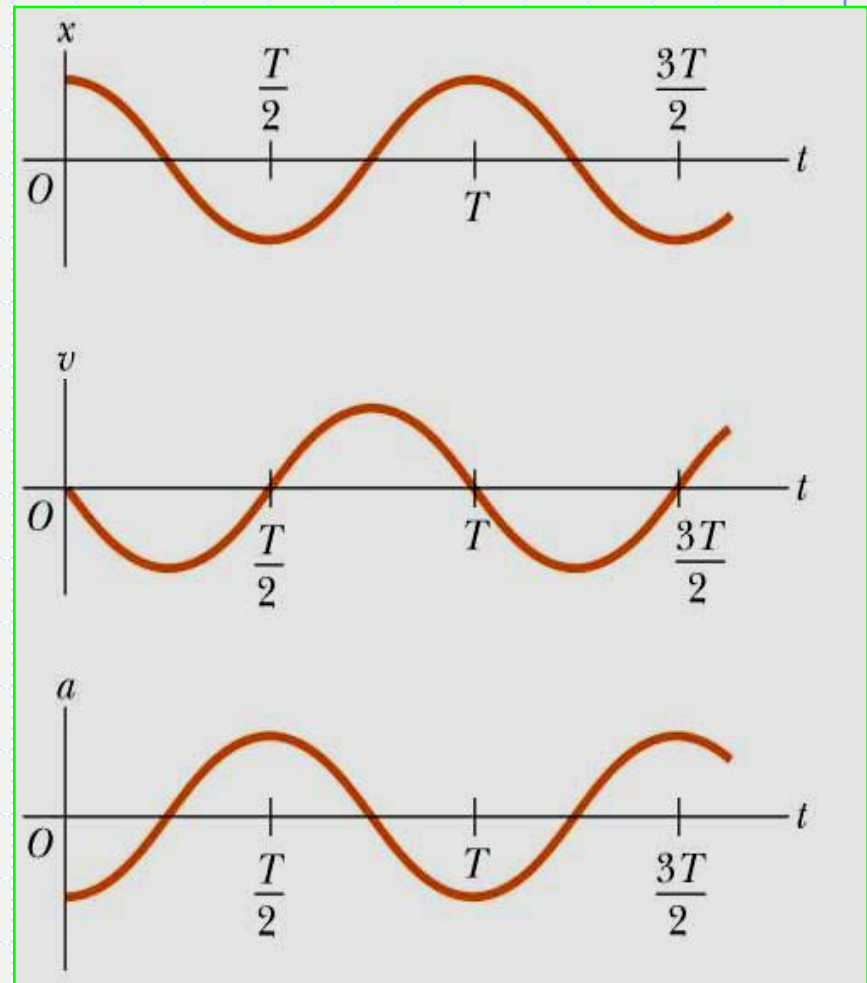


- ◆ The graphs show:
 - (a) displacement as a function of time
 - (b) velocity as a function of time
 - (c) acceleration as a function of time
- ◆ The velocity is 90° out of phase with the displacement and the acceleration is 180° out of phase with the displacement



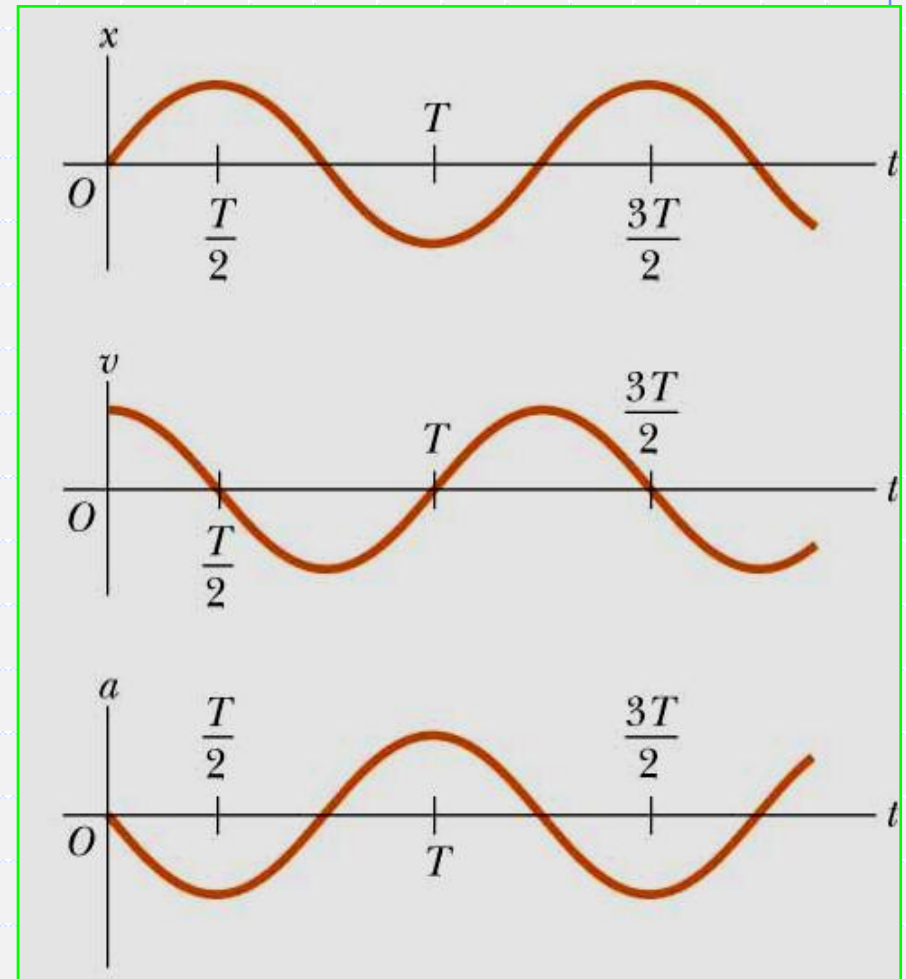
SHM Example 1

- ◆ Initial conditions at $t = 0$ are
 - $x(0) = A$
 - $v(0) = 0$
- ◆ This means $\phi = 0$
- ◆ The acceleration reaches extremes of $\pm \omega^2 A$
- ◆ The velocity reaches extremes of $\pm \omega A$

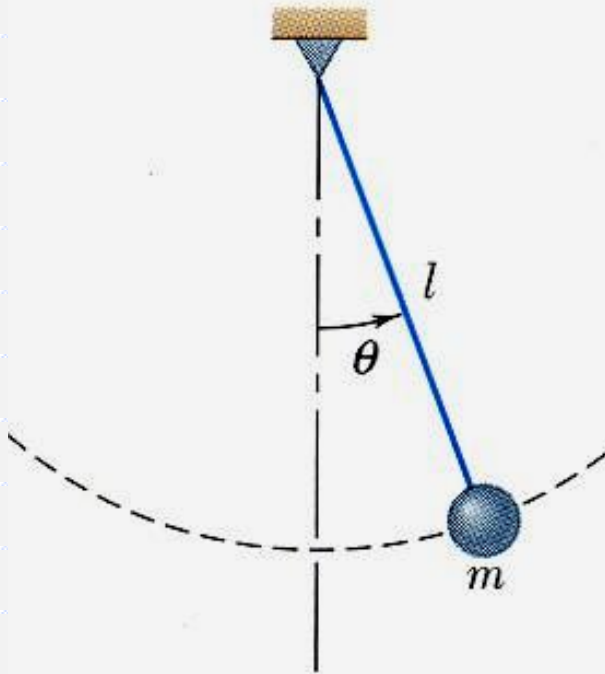


SHM Example 2

- ◆ Initial conditions at $t = 0$ are
 - $x(0) = 0$
 - $v(0) = v_i$
- ◆ This means $\phi = -\pi/2$
- ◆ The graph is shifted one-quarter cycle to the right compared to the graph of $x(0) = A$



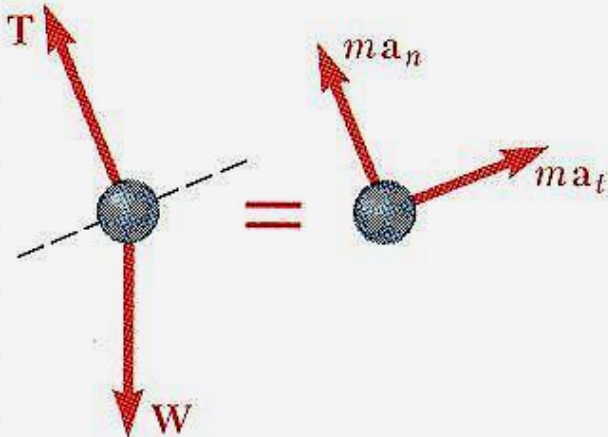
Simple Pendulum (Approximate Solution)



- Results obtained for the spring-mass system can be applied whenever the resultant force on a particle is proportional to the displacement and directed towards the equilibrium position.
- Consider tangential components of acceleration and force for a simple pendulum,

$$\sum F_t = m a_t$$

$$-W \sin \theta = ml\ddot{\theta}$$
$$\ddot{\theta} + \frac{g}{l} \sin \theta = 0$$



for small angles,

$$\omega_n = \sqrt{\frac{g}{l}}$$

$$\ddot{\theta} + \frac{g}{l} \theta = 0$$
$$\theta = \theta_m \sin(\omega_n t + \phi)$$
$$\tau_n = \frac{2\pi}{\omega_n} = 2\pi \sqrt{\frac{l}{g}}$$

Simple Pendulum (Exact Solution)

An exact solution for

$$\ddot{\theta} + \frac{g}{l} \sin \theta = 0$$

leads to

$$\tau_n = 4 \sqrt{\frac{l}{g}} \int_0^{\pi/2} \frac{d\phi}{\sqrt{1 - \sin^2(\theta_m/2) \sin^2 \phi}}$$

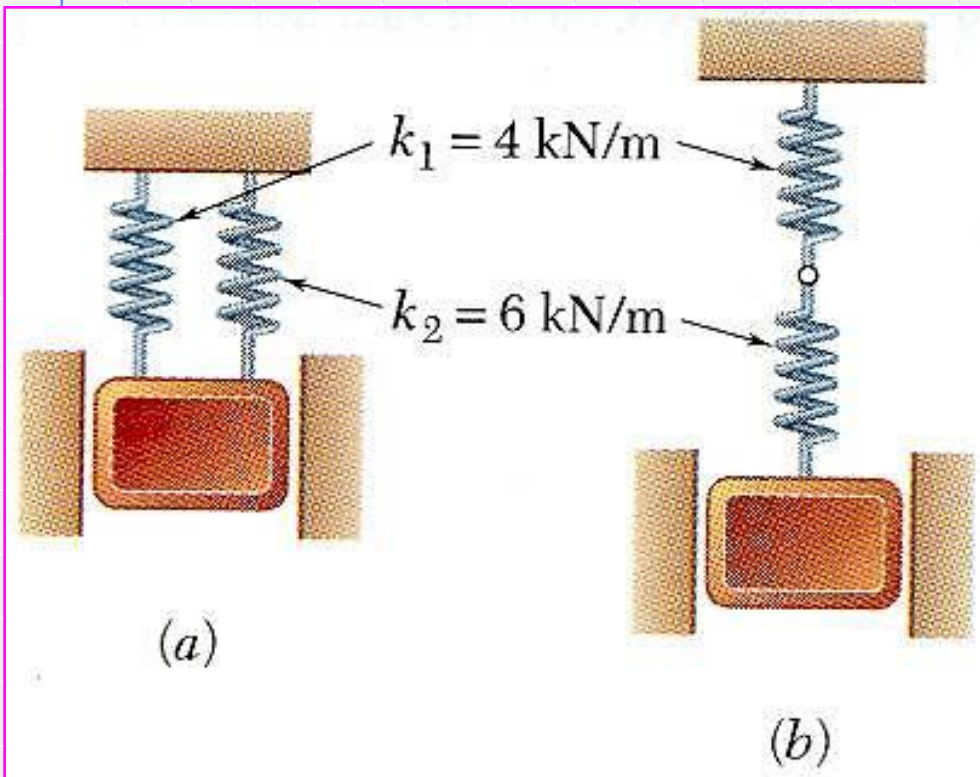
which requires numerical solution.

$$\tau_n = \frac{2K}{\pi} \left(2\pi \sqrt{\frac{l}{g}} \right)$$

Table 19.1. Correction Factor for the Period of a Simple Pendulum

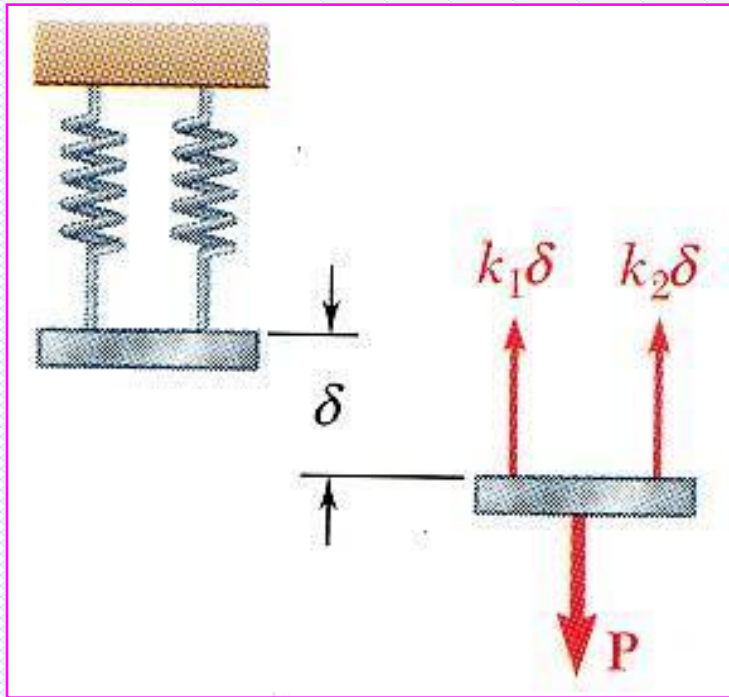
θ_m	0°	10°	20°	30°	60°	90°	120°	150°	180°
K	1.571	1.574	1.583	1.598	1.686	1.854	2.157	2.768	∞
$2K/\pi$	1.000	1.002	1.008	1.017	1.073	1.180	1.373	1.762	∞

مثال: بلوک 50 کیلوگرمی در دو سیستم متفاوت به دو فنر متصل گردیده است. اگر بلوک به اندازه 40 میلیمتر از حالت تعادل به سمت پائین کشیده و رها گردد: مطلوبست: الف) فرکانس هر یک از سیستم ها، ب) حداکثر سرعت بلوک و ج) حداکثر شتاب بلوک



- For each spring arrangement, determine the spring constant for a single equivalent spring.
- Apply the approximate relations for the harmonic motion of a spring-mass system.

$$k_1 = 4 \text{ kN/m} \quad k_2 = 6 \text{ kN/m}$$



$$P = k_1\delta + k_2\delta$$

$$k = \frac{P}{\delta} = k_1 + k_2$$

$$= 10 \text{ kN/m} = 10^4 \text{ N/m}$$

$$\omega_n = \sqrt{\frac{k}{m}} = \sqrt{\frac{10^4}{20}} = 14.14 \text{ rad/s}$$

$$\tau_n = \frac{2\pi}{\omega_n} = 0.444 \text{ (sec.)}$$

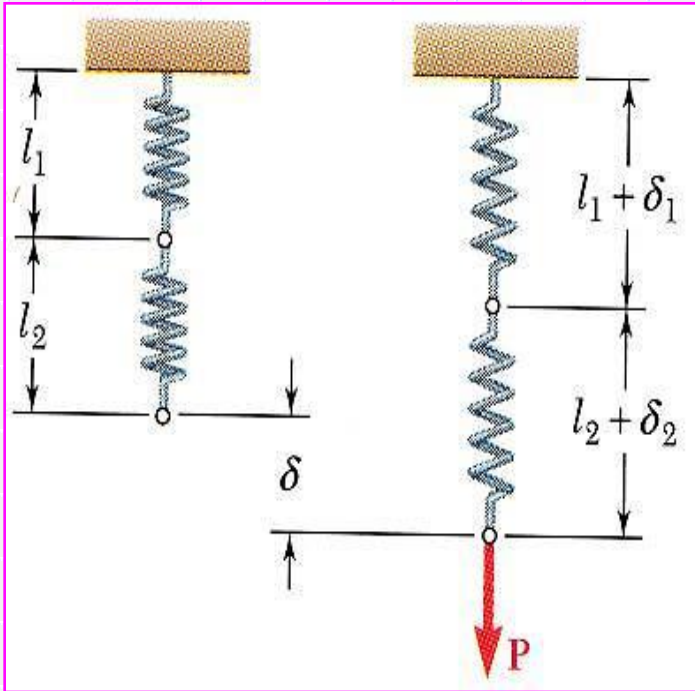
$$v_m = x_m \omega_n$$

$$= (0.040)(14.14) = 0.566 \text{ (m/s)}$$

$$a_m = x_m a_n^2$$

$$= (0.040)(14.14)^2 = 8 \text{ (m/s}^2\text{)}$$

$$k_1 = 4 \text{ kN/m} \quad k_2 = 6 \text{ kN/m}$$



$$\omega_n = \sqrt{\frac{k}{m}} = \sqrt{\frac{2400 \text{ N/m}}{20 \text{ kg}}} = 6.93 \text{ rad/s}$$

$$\tau_n = \frac{2\pi}{\omega_n} = 0.907 \text{ (sec.)}$$

$$v_m = x_m \omega_n$$

$$= (0.040)(6.93) = 0.277 \text{ (m/s)}$$

$$a_m = x_m a_n^2$$

$$= (0.040)(6.93)^2 = 1.92 \text{ (m/s}^2\text{)}$$

$$\delta = \delta_1 + \delta_2 = \frac{P}{k_1} + \frac{P}{k_2}$$

$$k = \frac{P}{\delta} = \frac{P}{\frac{P}{k_1} + \frac{P}{k_2}} = \frac{k_1 k_2}{k_1 + k_2}$$

$$= 2400 \text{ N/m}$$

Free Vibrations of Rigid Body

ارتعاش آزاد جسم صلب

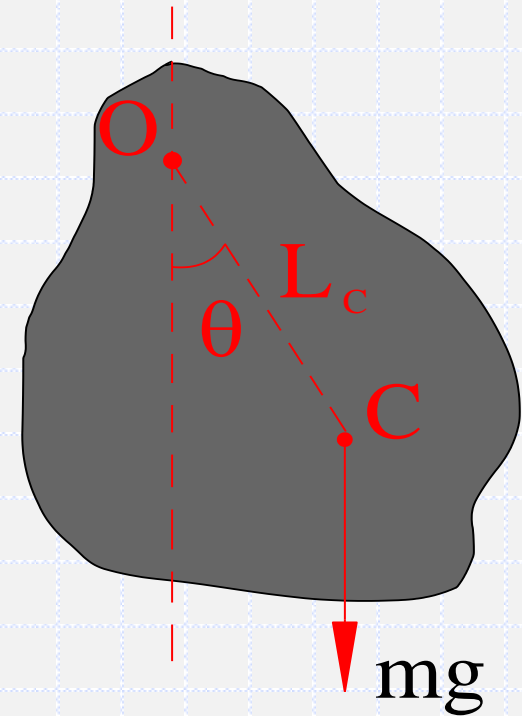
→ $-mg \sin \theta l_c = I_o \alpha$

→ for small angles $\sin \theta \approx \theta$

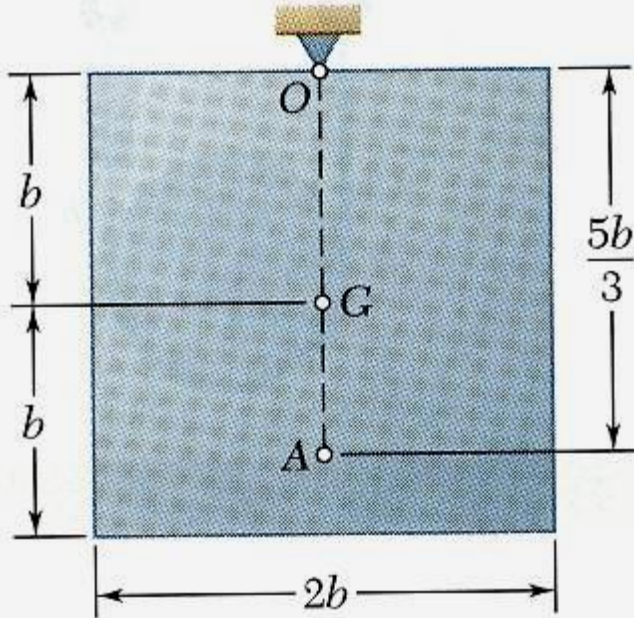
→ $-mg \theta l_c = I_o \ddot{\theta}$

→ $\ddot{\theta} + \frac{mgl_c}{I_o} \theta = 0$

→ $\ddot{\theta} + \omega^2 \theta = 0$



Free Vibrations of Rigid Body ارتعاش آزاد جسم صلب



- If an equation of motion takes the form

$$\ddot{x} + \omega_n^2 x = 0 \quad \text{or} \quad \ddot{\theta} + \omega_n^2 \theta = 0$$

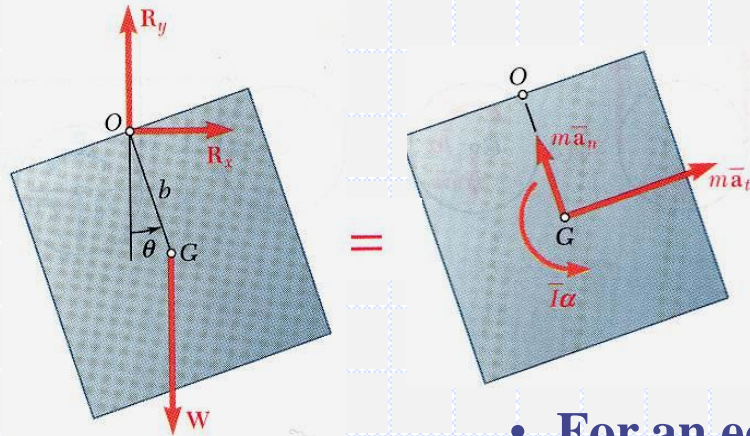
- the corresponding motion may be considered as simple harmonic motion.
- Analysis objective is to determine ω_n .
- Consider the oscillations of a square plate

$$\sum \bar{M}_O = 0 \Rightarrow -W(b \sin \theta) = (mb \ddot{\theta}) + \bar{I} \ddot{\theta}$$

$$\text{but } \bar{I} = \frac{1}{12} m [(2b)^2 + (2b)^2] = \frac{2}{3} mb^2, \quad W = mg$$

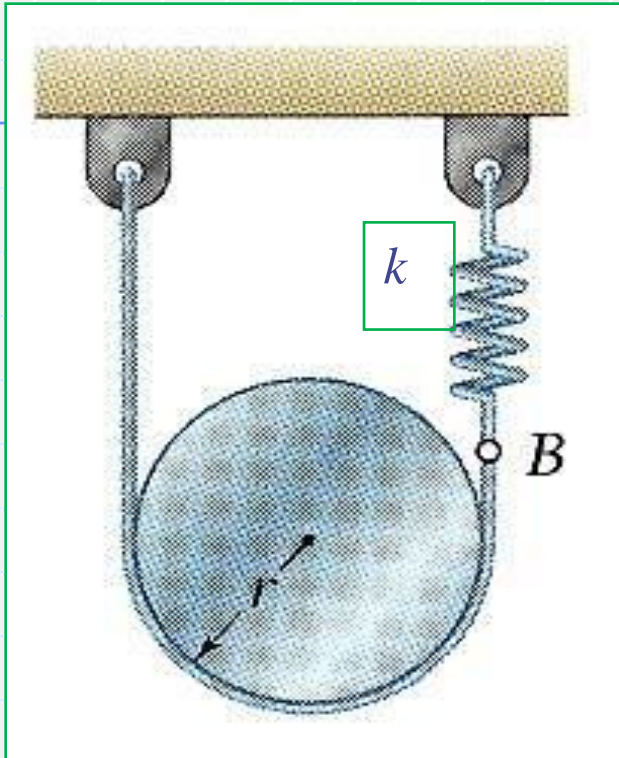
$$\ddot{\theta} + \frac{3g}{5b} \sin \theta \cong \ddot{\theta} + \frac{3g}{5b} \theta = 0$$

$$\text{then } \omega_n = \sqrt{\frac{3g}{5b}}, \quad \tau_n = \frac{2\pi}{\omega_n} = 2\pi \sqrt{\frac{5b}{3g}}$$

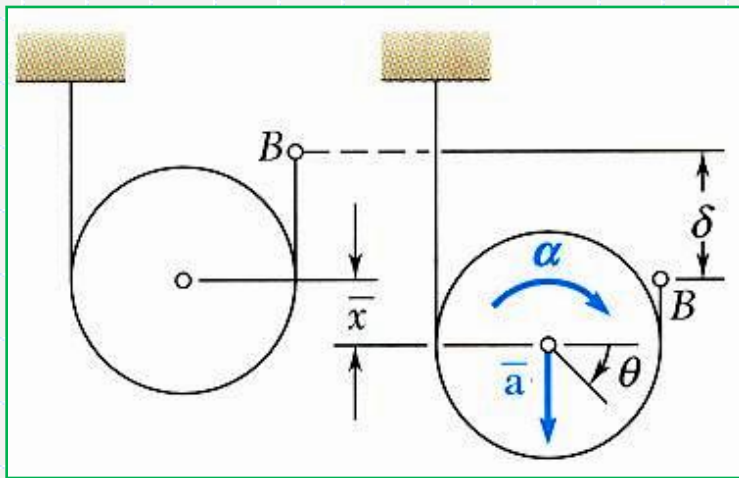


- For an equivalent simple pendulum, $l = 5b/3$

مثال: دیسک با وزن W به حالت نشان داده شده معلق نگهداشته شده است که رها می‌گردد. مطلوبست: فرکانس طبیعی دیسک.



- From the kinematics of the system, relate the linear displacement and acceleration to the rotation of the cylinder.
- Based on a free-body-diagram equation for the equivalence of the external and effective forces, write the equation of motion.
- Substitute the kinematic relations to arrive at an equation involving only the angular displacement and acceleration.



$$\bar{x} = r\theta$$

$$\delta = 2\bar{x} = 2r\theta$$

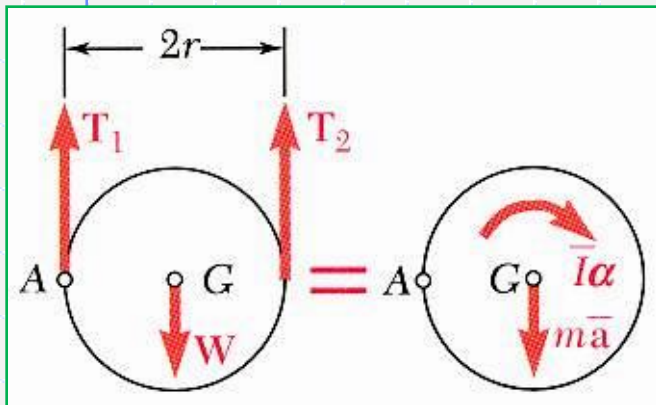
$$\bar{a} = \ddot{\theta} \uparrow$$

$$\bar{a} = r\alpha = r\ddot{\theta}$$

$$\vec{a} = r\ddot{\theta} \uparrow \downarrow$$

$$\uparrow \sum M_A = \sum (M_A)_{eff} : \quad Wr - T_2(2r) = m\bar{a}r + \bar{I}\alpha$$

$$\text{but } T_2 = T_0 + k\delta = \frac{1}{2}W + k(2r\theta)$$



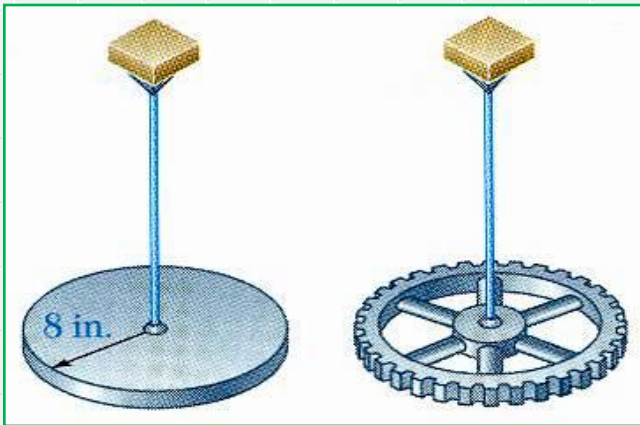
$$Wr - \left(\frac{1}{2}W + 2kr\theta \right) (2r) = m(r\ddot{\theta})r + \frac{1}{2}mr^2\ddot{\theta}$$

$$\ddot{\theta} + \frac{8k}{3m}\theta = 0$$

$$\omega_n = \sqrt{\frac{8k}{3m}}$$

$$\tau_n = \frac{2\pi}{\omega_n} = 2\pi\sqrt{\frac{3m}{8k}}$$

$$f_n = \frac{\omega_n}{2\pi} = \frac{1}{2\pi}\sqrt{\frac{8k}{3m}}$$



$$W = 20 \text{ lb}$$

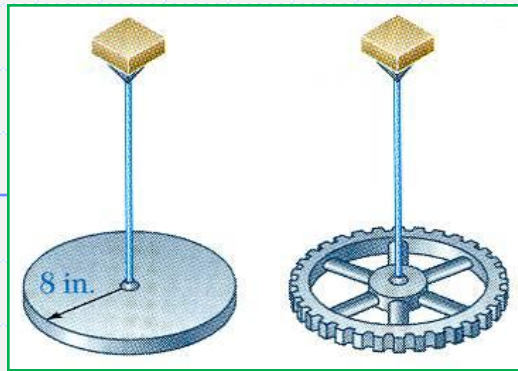
$$\tau_n = 1.13 \text{ s}$$

$$\tau_n = 1.93 \text{ s}$$

The disk and gear undergo torsional vibration with the periods shown. Assume that the moment exerted by the wire is proportional to the twist angle.

Determine *a)* the wire torsional spring constant, *b)* the centroidal moment of inertia of the gear, and *c)* the maximum angular velocity of the gear if rotated through 90° and released.

- Using the free-body-diagram equation for the equivalence of the external and effective moments, write the equation of motion for the disk/gear and wire.
- With the natural frequency and moment of inertia for the disk known, calculate the torsional spring constant.
- With natural frequency and spring constant known, calculate the moment of inertia for the gear.
- Apply the relations for simple harmonic motion to calculate the maximum gear velocity.



$W = 20 \text{ lb}$

$\tau_n = 1.13 \text{ s}$

$\tau_n = 1.93 \text{ s}$

SOLUTION:

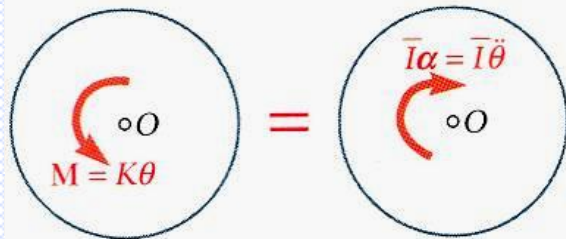
- Using the free-body-diagram equation for the equivalence of the external and effective moments, write the equation of motion for the disk/gear and wire.

$$+\curvearrowright \sum M_O = \sum (M_O)_{eff} :$$

$$+ K\theta = -\bar{I}\ddot{\theta}$$

$$\ddot{\theta} + \frac{K}{\bar{I}}\theta = 0$$

$$\omega_n = \sqrt{\frac{K}{\bar{I}}} \quad \tau_n = \frac{2\pi}{\omega_n} = 2\pi\sqrt{\frac{\bar{I}}{K}}$$

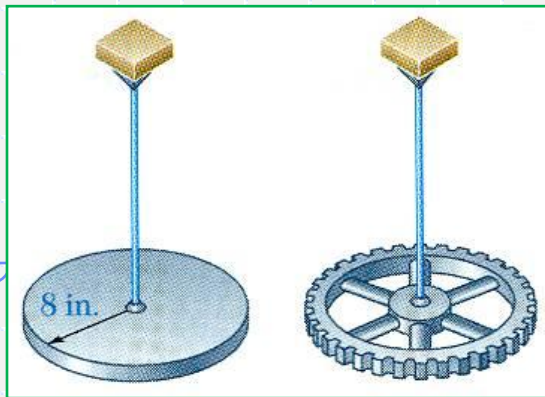


- With the natural frequency and moment of inertia for the disk known, calculate the torsional spring constant.

$$\bar{I} = \frac{1}{2}mr^2 = \frac{1}{2}\left(\frac{20}{32.2}\right)\left(\frac{8}{12}\right)^2 = 0.138 \text{ lb} \cdot \text{ft} \cdot \text{s}^2$$

$$1.13 = 2\pi\sqrt{\frac{0.138}{K}}$$

$$K = 4.27 \text{ lb} \cdot \text{ft}/\text{rad}$$



$$W = 20 \text{ lb}$$

$$\tau_n = 1.13 \text{ s}$$

$$\tau_n = 1.93 \text{ s}$$

- With natural frequency and spring constant known, calculate the moment of inertia for the gear.

$$1.93 = 2\pi \sqrt{\frac{\bar{I}}{4.27}}$$

$$\bar{I} = 0.403 \text{ lb} \cdot \text{ft} \cdot \text{s}^2$$

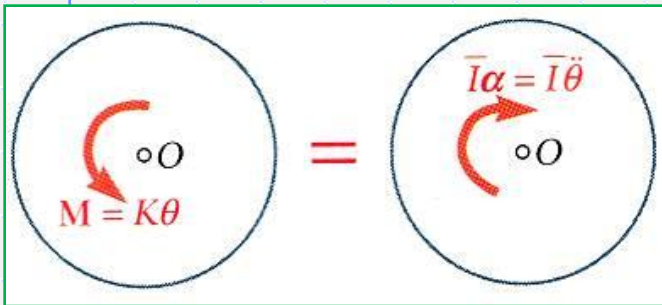
- Apply the relations for simple harmonic motion to calculate the maximum gear velocity.

$$\theta = \theta_m \sin \omega_n t \quad \omega = \theta_m \omega_n \sin \omega_n t \quad \omega_m = \theta_m \omega_n$$

$$\theta_m = 90^\circ = 1.571 \text{ rad}$$

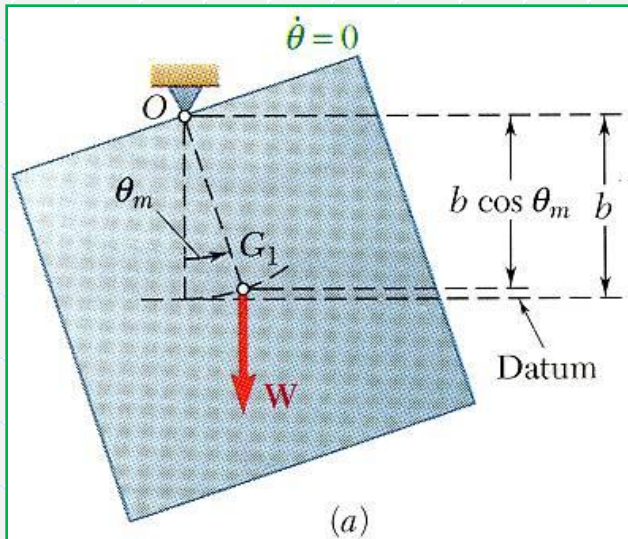
$$\omega_m = \theta_m \left(\frac{2\pi}{\tau_n} \right) = (1.571 \text{ rad}) \left(\frac{2\pi}{1.93 \text{ s}} \right)$$

$$\omega_m = 5.11 \text{ rad/s}$$



Principle of Conservation of Energy

اصل حفظ انرژی مکانیکی

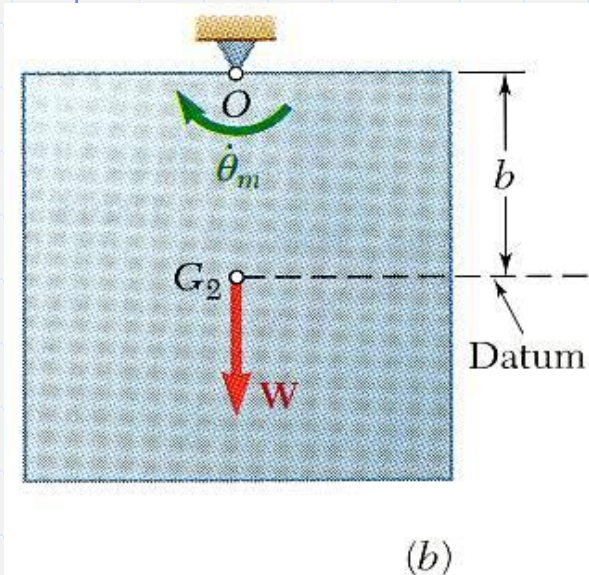


$$T + V = \text{const.} \quad \frac{1}{2} m \dot{x}^2 + \frac{1}{2} k x^2 = \text{const.}$$

$$\dot{x}^2 + \omega_n^2 x^2 =$$

$$T_1 = 0 \quad V_1 = Wb(1 - \cos\theta) = Wb \left[2 \sin^2(\theta_m/2) \right]$$

$$\cong \frac{1}{2} Wb \theta_m^2$$



$$T_2 = \frac{1}{2} m \bar{v}_m^2 + \frac{1}{2} \bar{I} \omega_m^2$$

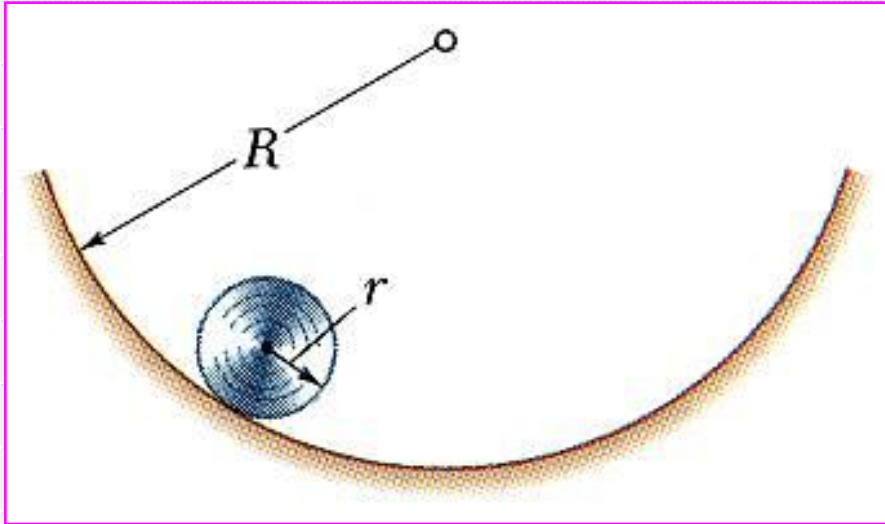
$$= \frac{1}{2} m (b \dot{\theta}_m)^2 + \frac{1}{2} \left(\frac{2}{3} m b^2 \right) \omega_m^2$$

$$= \frac{1}{2} \left(\frac{5}{3} m b^2 \right) \dot{\theta}_m^2$$

$$V_2 = 0$$

$$T_1 + V_1 = T_2 + V_2$$

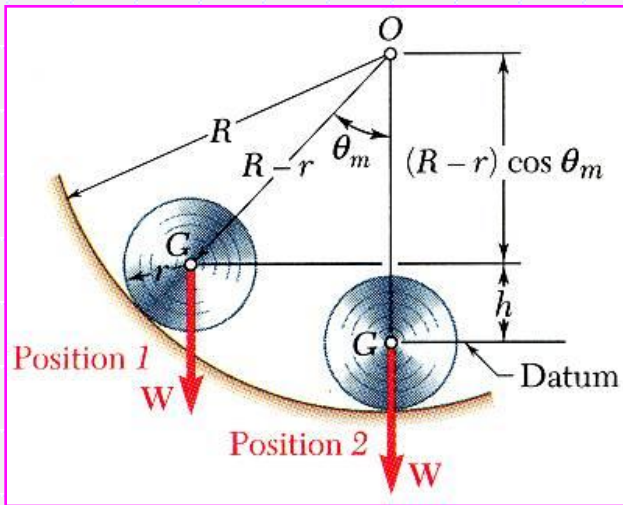
$$0 + \frac{1}{2} Wb \theta_m^2 = \frac{1}{2} \left(\frac{5}{3} m b^2 \right) \theta_m^2 \omega_n^2 + 0 \quad \omega_n = \sqrt{3g/5b}$$



Determine the period of small oscillations of a cylinder which rolls without slipping inside a curved surface.

SOLUTION:

- Apply the principle of conservation of energy between the positions of maximum and minimum potential energy.
- Solve the energy equation for the natural frequency of the oscillations.



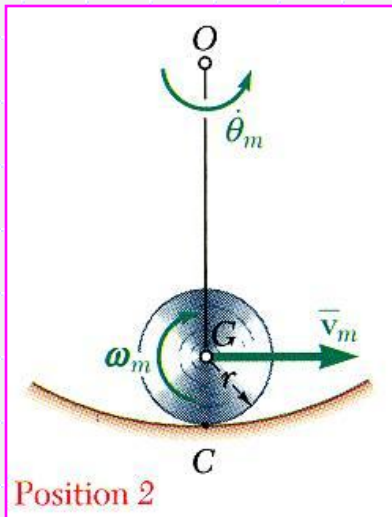
SOLUTION:

- Apply the principle of conservation of energy between the positions of maximum and minimum potential energy.

$$T_1 + V_1 = T_2 + V_2$$

$$T_1 = 0$$

$$V_1 = Wh = W(R-r)(1 - \cos\theta) \cong W(R-r)\left(\frac{\theta_m^2}{2}\right)$$

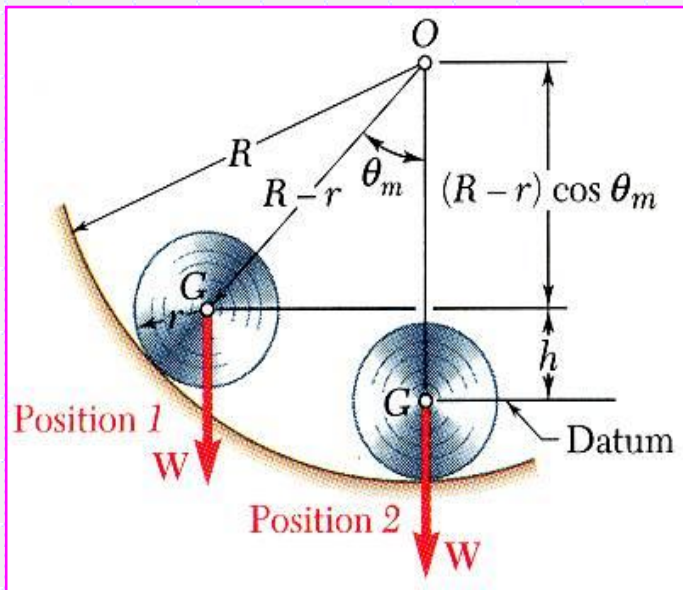


$$T_2 = \frac{1}{2} m \bar{v}_m^2 + \frac{1}{2} \bar{I} \omega_m^2$$

$$V_2 = 0$$

$$= \frac{1}{2} m (R-r) \dot{\theta}_m^2 + \frac{1}{2} \left(\frac{1}{2} m r^2 \right) \left(\frac{R-r}{r} \right)^2 \dot{\theta}_m^2$$

$$= \frac{3}{4} m (R-r)^2 \dot{\theta}_m^2$$



- Solve the energy equation for the natural frequency of the oscillations.

$$T_1 + V_1 = T_2 + V_2$$

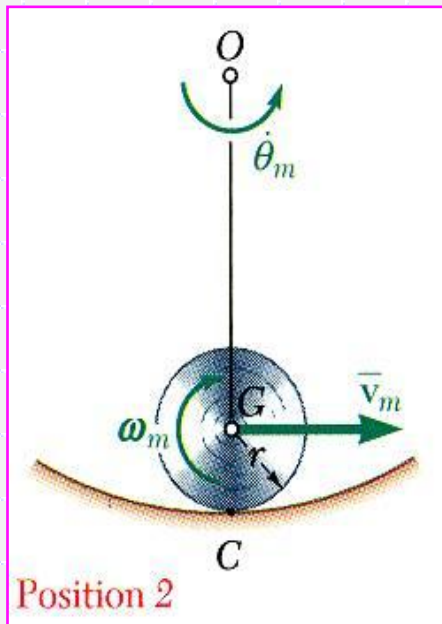
$$T_1 = 0$$

$$V_1 \cong W(R-r)\left(\frac{\theta_m^2}{2}\right)$$

$$T_2 = \frac{3}{4}m(R-r)^2\dot{\theta}_m^2 \quad V_2 = 0$$

$$0 + W(R-r)\frac{\theta_m^2}{2} = \frac{3}{4}m(R-r)^2\dot{\theta}_m^2 + 0$$

$$(mg)(R-r)\frac{\theta_m^2}{2} = \frac{3}{4}m(R-r)^2(\theta_m\omega_n)^2$$



$$\omega_n^2 = \frac{2}{3} \frac{g}{R-r}$$

$$\tau_n = \frac{2\pi}{\omega_n} = 2\pi \sqrt{\frac{3}{2} \frac{R-r}{g}}$$

Forced Vibrations

ارتعاش زوری (با نیروی خارجی)

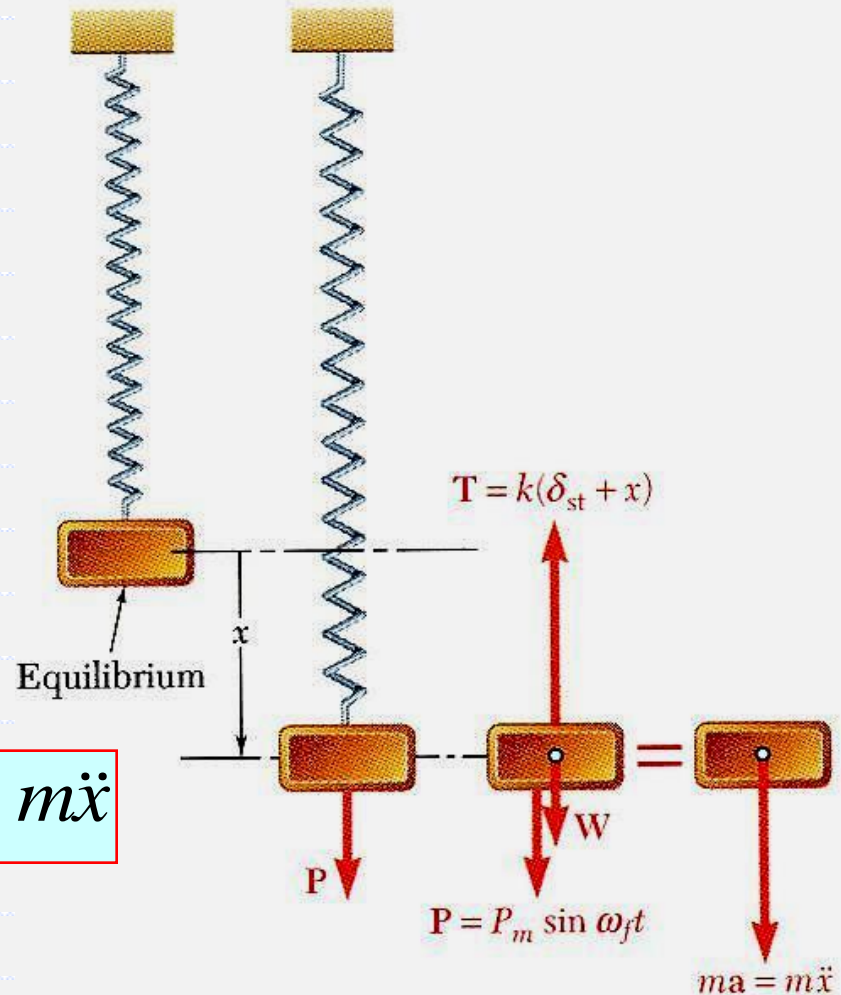
Forced vibrations - Occur when a system is subjected to a periodic force or a periodic displacement of a support.

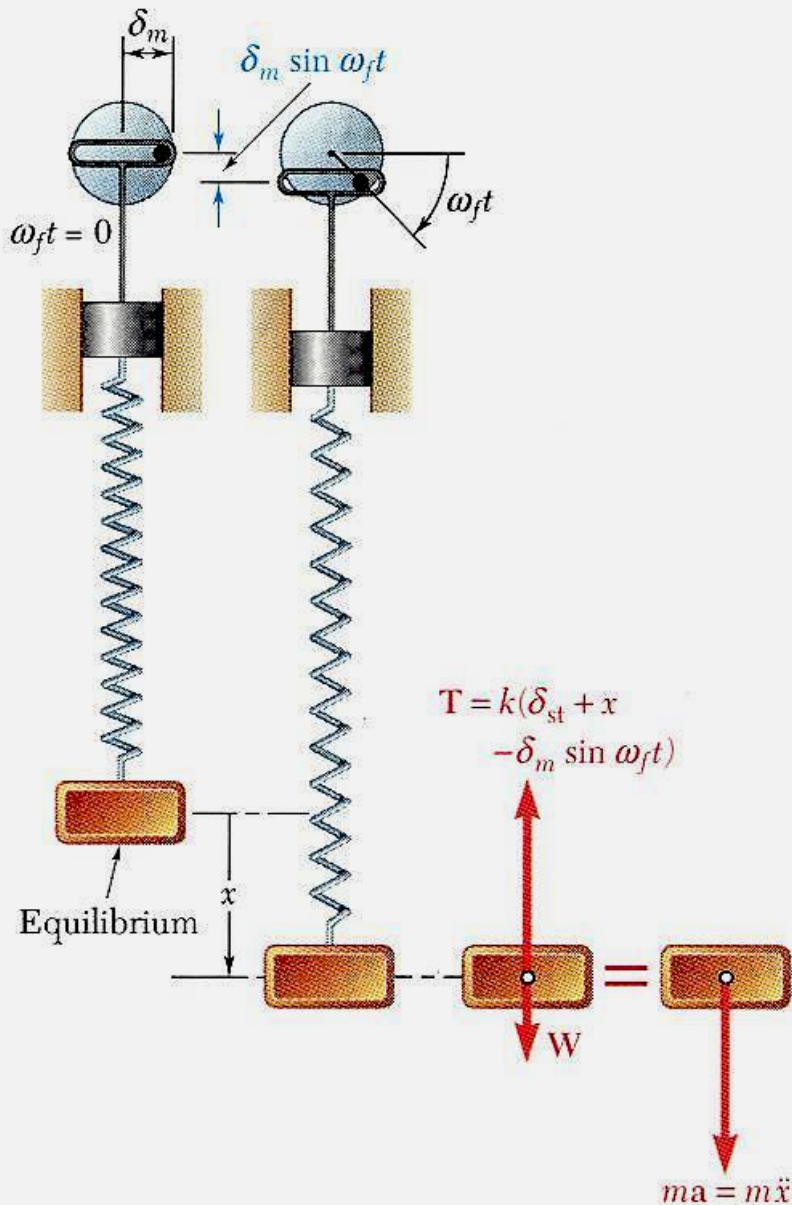
$\omega_f = \text{forced frequency}$

$$+\downarrow \sum F = ma :$$

$$P_m \sin \omega_f t + W - k(\delta_{st} + x) = m\ddot{x}$$

$$m\ddot{x} + kx = P_m \sin \omega_f t$$





$\omega_f = \text{forced frequency}$

$$+\downarrow \sum F = ma :$$

$$W - k(\delta_{st} + x - \delta_m \sin \omega_f t) = m\ddot{x}$$

$$m\ddot{x} + kx = k\delta_m \sin \omega_f t$$

$$m\ddot{x} + kx = P_m \sin \omega_f t$$

$$m\ddot{x} + kx = k\delta_m \sin \omega_f t$$

$$x = x_{comp.} + x_{part.}$$

$$= [A \sin \omega_n t + B \cos \omega_n t] + x_m \sin \omega_f t$$

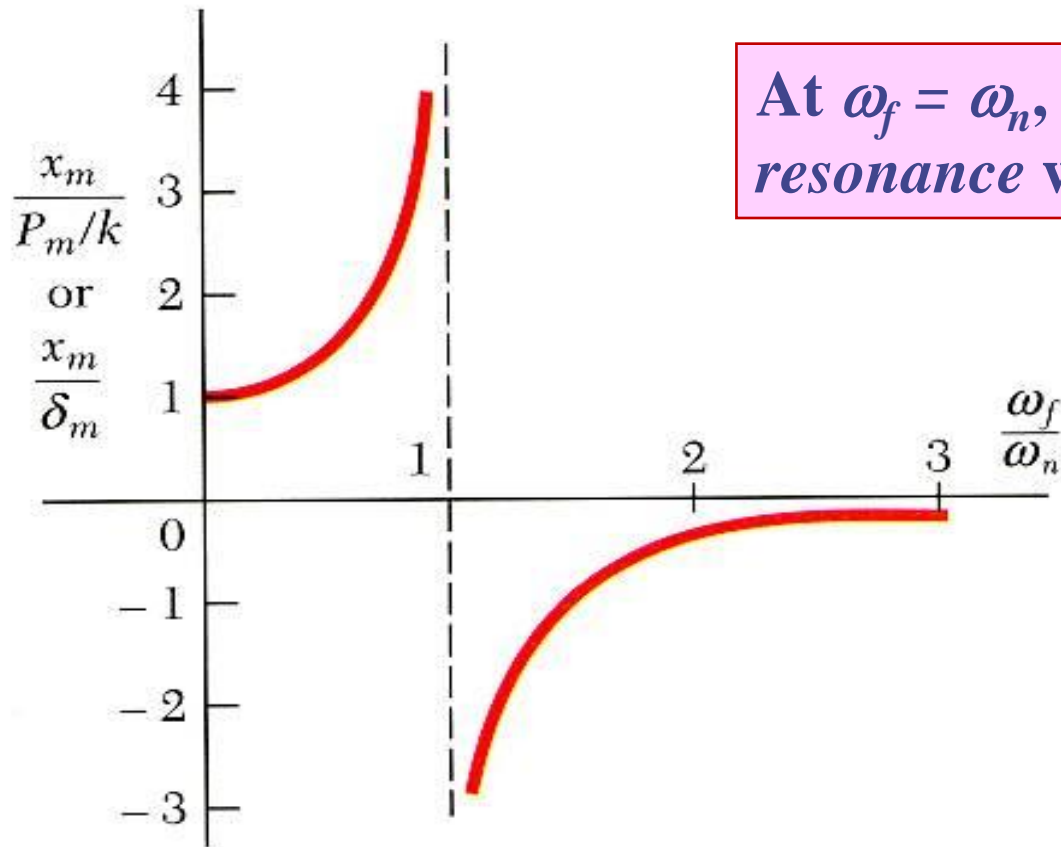
Substituting particular solution into governing equation,

$$-m\omega_f^2 x_m \sin \omega_f t + kx_m \sin \omega_f t = P_m \sin \omega_f t$$

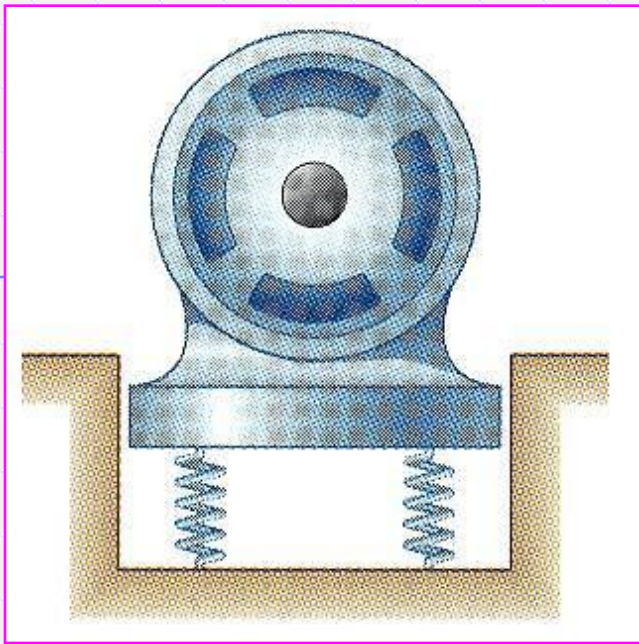
$$x_m = \frac{P_m}{k - m\omega_f^2} = \frac{P_m/k}{1 - (\omega_f/\omega_n)^2} = \frac{\delta_m}{1 - (\omega_f/\omega_n)^2}$$

$$\begin{aligned} \text{Magnification factor} &= \frac{x_m}{P_m/k} = \frac{x_m}{\delta_m} \\ &= \frac{1}{1 - (\omega_f/\omega_n)^2} \end{aligned}$$

$$\begin{aligned} \text{Magnification factor} &= \frac{x_m}{P_m/k} = \frac{x_m}{\delta_m} \\ &= \frac{1}{1 - (\omega_f/\omega_n)^2} \end{aligned}$$



At $\omega_f = \omega_n$, forcing input is in *resonance* with the system.

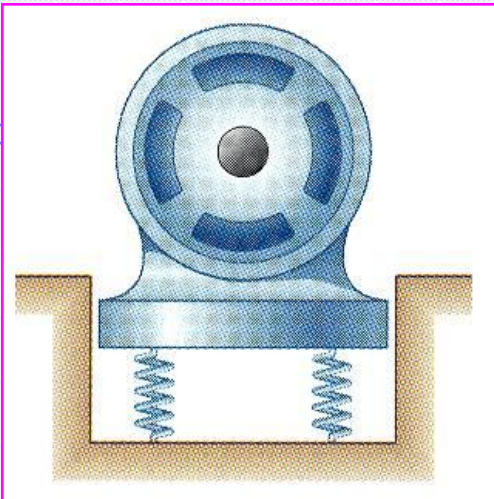


A motor weighing 350 lb is supported by four springs, each having a constant 750 lb/in. The unbalance of the motor is equivalent to a weight of 1 oz located 6 in. from the axis of rotation.

Determine *a)* speed in rpm at which resonance will occur, and *b)* amplitude of the vibration at 1200 rpm.

SOLUTION:

- The resonant frequency is equal to the natural frequency of the system.
- Evaluate the magnitude of the periodic force due to the motor unbalance. Determine the vibration amplitude from the frequency ratio at 1200 rpm.



$$W = 350 \text{ lb}$$

$$k = 4(750 \text{ lb/in})$$

SOLUTION:

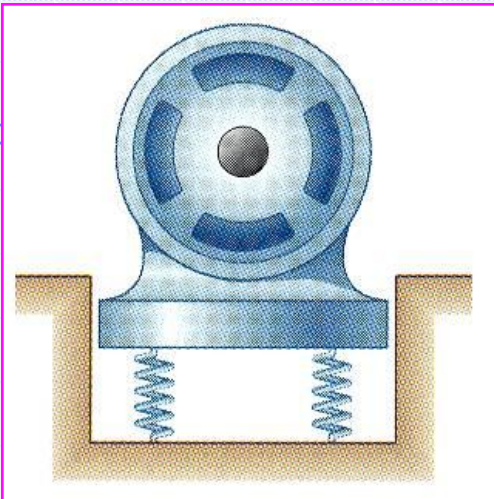
- The resonant frequency is equal to the natural frequency of the system.

$$m = \frac{350}{32.2} = 10.87 \text{ lb} \cdot \text{s}^2/\text{ft}$$

$$\begin{aligned} k &= 4(750) = 3000 \text{ lb/in} \\ &= 36,000 \text{ lb/ft} \end{aligned}$$

$$\begin{aligned} \omega_n &= \sqrt{\frac{k}{m}} = \sqrt{\frac{36,000}{10.87}} \\ &= 57.5 \text{ rad/s} = 549 \text{ rpm} \end{aligned}$$

Resonance speed = 549 rpm



$$W = 350 \text{ lb}$$

$$k = 4(750 \text{ lb/in})$$

$$\omega_n = 57.5 \text{ rad/s}$$

- Evaluate the magnitude of the periodic force due to the motor unbalance. Determine the vibration amplitude from the frequency ratio at 1200 rpm.

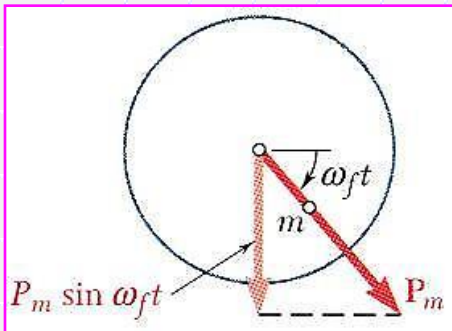
$$\omega_f = \omega = 1200 \text{ rpm} = 125.7 \text{ rad/s}$$

$$m = (1 \text{ oz}) \left(\frac{1 \text{ lb}}{16 \text{ oz}} \right) \left(\frac{1}{32.2 \text{ ft/s}^2} \right) = 0.001941 \text{ lb} \cdot \text{s}^2/\text{ft}$$

$$P_m = ma_n = mr\omega^2 = (0.001941) \left(\frac{6}{12} \right) (125.7)^2 = 15.33 \text{ lb}$$

$$x_m = \frac{P_m/k}{1 - (\omega_f/\omega_n)^2} = \frac{15.33/3000}{1 - (125.7/57.5)^2} = -0.001352 \text{ in}$$

$$x_m = 0.001352 \text{ in. (out of phase)}$$



Damped Free Vibrations

ارتعاش آزاد با میرائی

- All vibrations are damped to some degree by forces due to *dry friction, fluid friction, or internal friction.*
- With viscous damping due to fluid friction,

$$+\downarrow \sum F = ma : \quad W - k(\delta_{st} + x) - c\dot{x} = m\ddot{x}$$

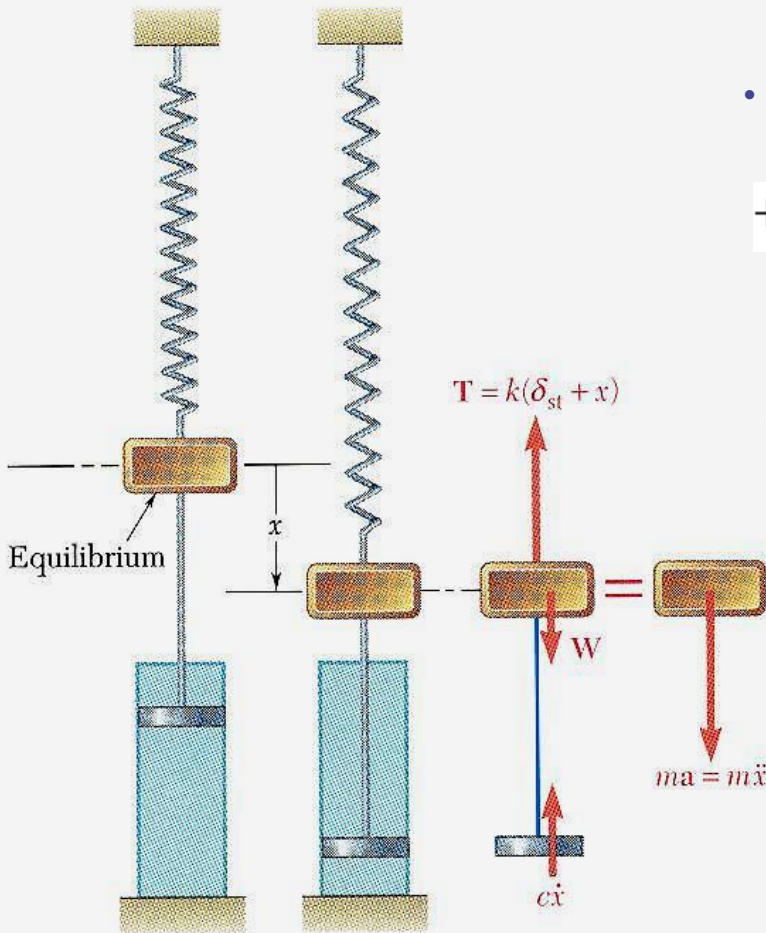
$$m\ddot{x} + c\dot{x} + kx = 0$$

- Substituting $x = e^{\lambda t}$ and dividing through by $e^{\lambda t}$ yields the characteristic equation,

$$m\lambda^2 + c\lambda + k = 0 \quad \lambda = -\frac{c}{2m} \pm \sqrt{\left(\frac{c}{2m}\right)^2 - \frac{k}{m}}$$

- Define the critical damping coefficient such that

$$\left(\frac{c_c}{2m}\right)^2 - \frac{k}{m} = 0 \quad c_c = 2m\sqrt{\frac{k}{m}} = 2m\omega_n$$



• **Characteristic equation :**

$$m\lambda^2 + c\lambda + k = 0 \quad \lambda = -\frac{c}{2m} \pm \sqrt{\left(\frac{c}{2m}\right)^2 - \frac{k}{m}}$$

$$c_c = 2m\omega_n = \text{critical damping coefficient}$$

- **Heavy damping : $c > c_c$**

$$x = Ae^{\lambda_1 t} + Be^{\lambda_2 t} \quad \begin{array}{l} \text{- negative roots} \\ \text{- nonvibratory motion} \end{array}$$

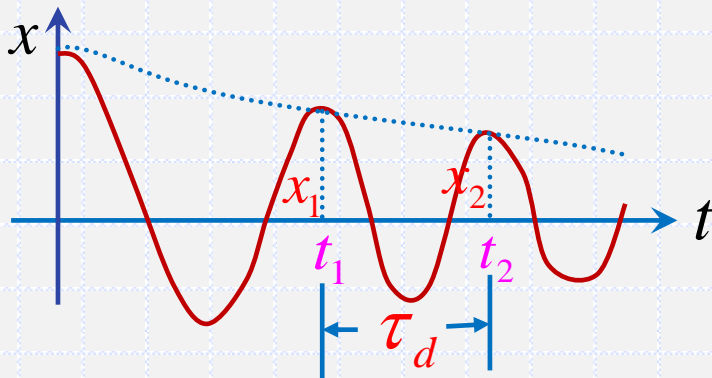
- **Critical damping : $c = c_c$**

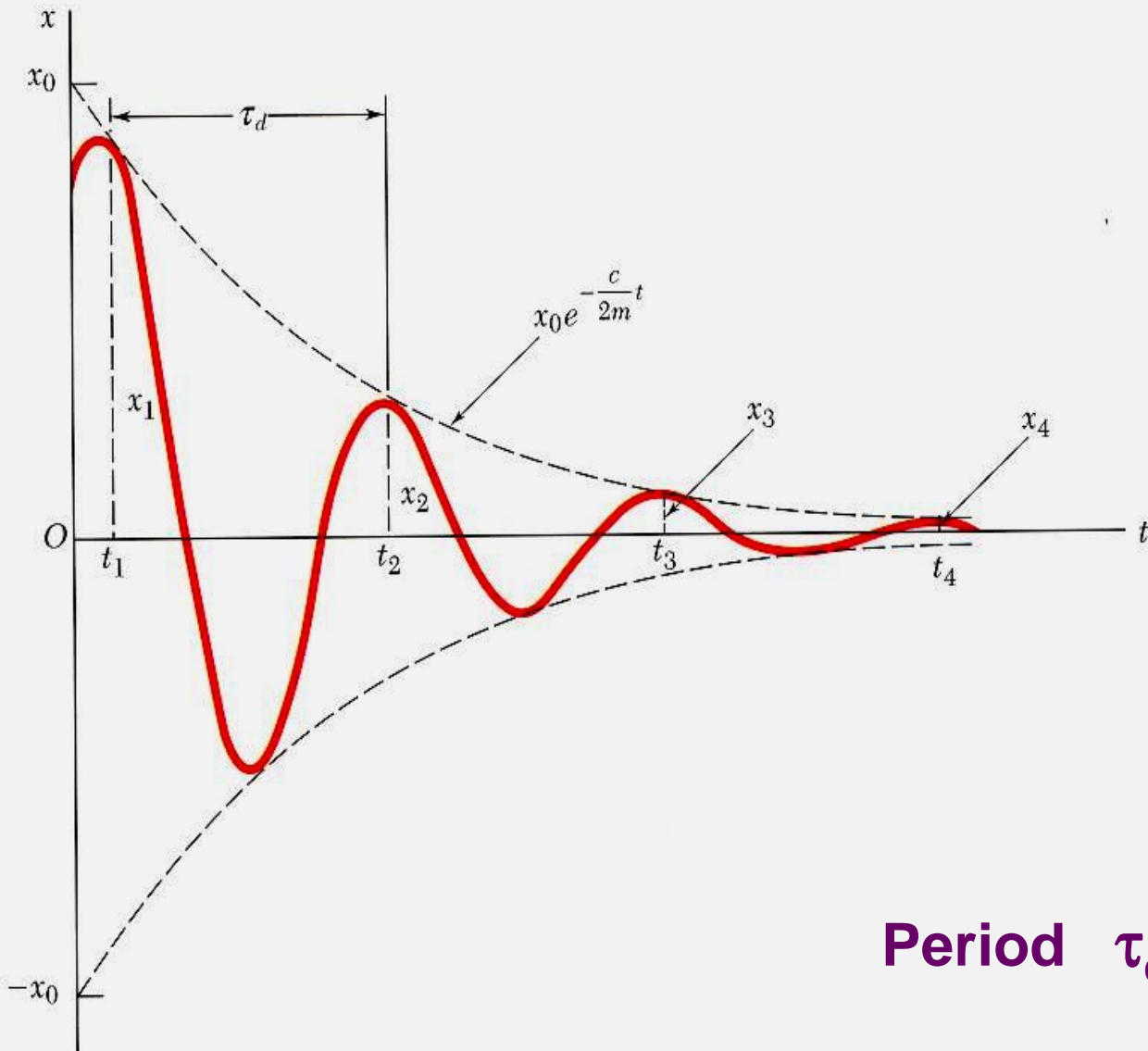
$$x = (A + Bt)e^{-\omega_n t} \quad \begin{array}{l} \text{- double roots} \\ \text{- nonvibratory motion} \end{array}$$

- **Light damping : $c < c_c$**

$$x = e^{-(c/2m)t} (A \sin \omega_d t + B \cos \omega_d t)$$

$$\omega_d = \omega_n \sqrt{1 - \left(\frac{c}{c_c}\right)^2} = \text{damped frequency}$$





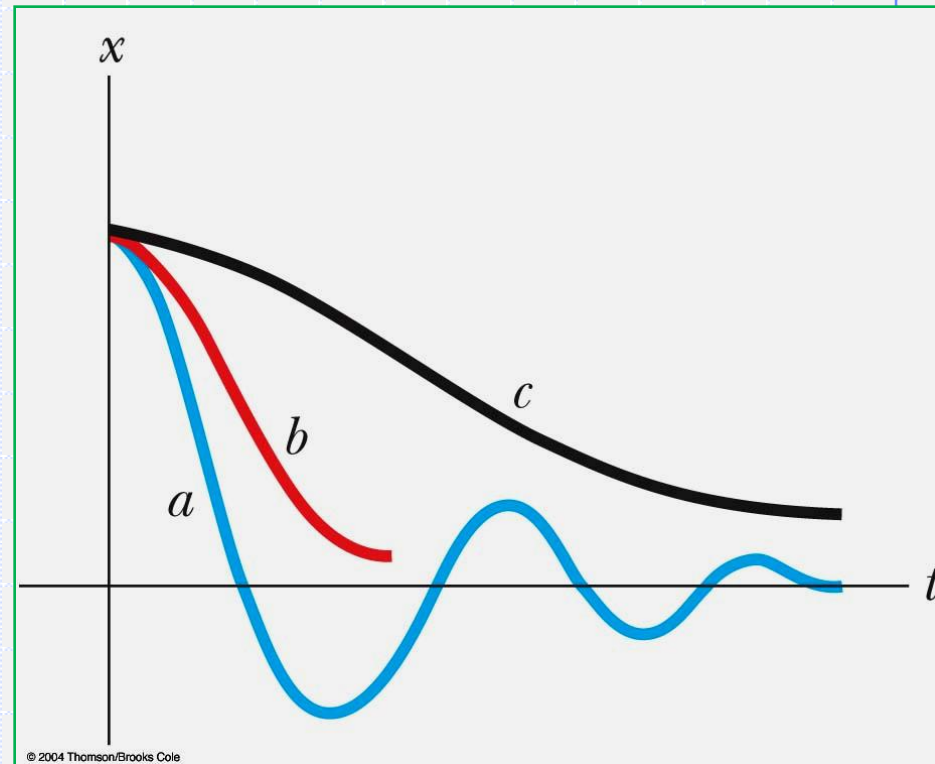
Period $\tau_d = 2\pi/\omega_d$

Types of Damping

◆ Graphs of position versus time for

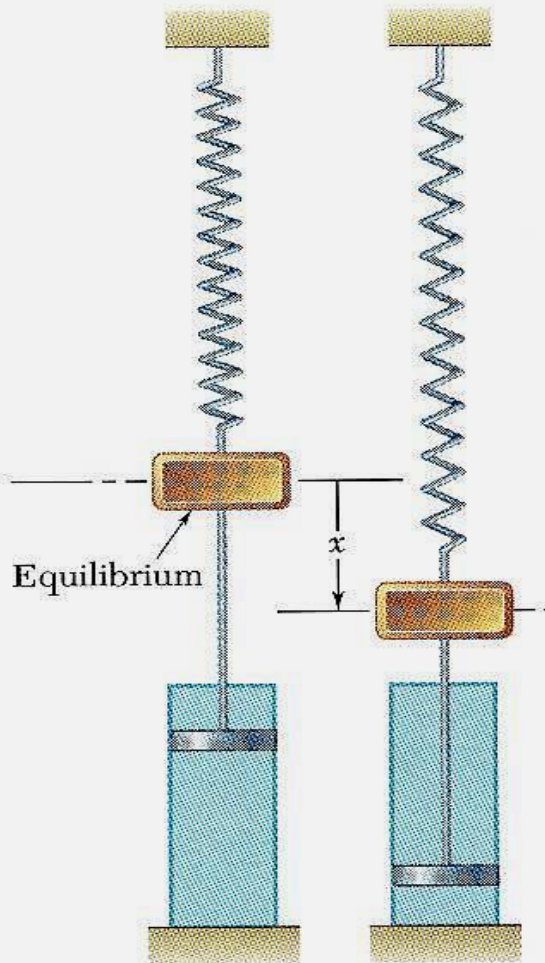
- (a) Light damped oscillator
- (b) a critically damped oscillator
- (c) Heavy damped oscillator

◆ For critically damped and heavy damped there is no angular frequency



Damped Forced Vibrations

ارتعاش زوری با میرائی



$$m\ddot{x} + c\dot{x} + kx = P_m \sin \omega_f t$$

$$x = x_{comp.} + x_{part.}$$

$$\frac{x_m}{P_m/k} = \frac{x_m}{\delta_m} = \frac{1}{\sqrt{[1 - (\omega_f/\omega_n)^2]^2 + [2(c/c_c)(\omega_f/\omega_n)]^2}}$$

$$\tan \varphi = \frac{2(c/c_c)(\omega_f/\omega_n)}{1 - (\omega_f/\omega_n)^2}$$

where $\omega_n = \sqrt{k/m}$ = natural circular frequency of undamped system

$c_c = 2m\omega_n$ = critical damping coefficient

c/c_c = damping factor

$$\frac{x_m}{P_m/k} = \frac{x_m}{\delta} = \frac{1}{\sqrt{[1 - (\omega_f/\omega_n)^2]^2 + [2(c/c_c)(\omega_f/\omega_n)]^2}} =$$

$$\tan \phi = \frac{2(c/c_c)(\omega_f/\omega_n)}{1 - (\omega_f/\omega_n)^2} =$$

magnification factor

phase difference between forcing and steady state response

